

Nonlinear Control

Lecture # 38

Tracking & Regulation

Output Feedback

Tracking:

$$\dot{\eta} = f_0(\eta, \xi)$$

$$\dot{e}_i = e_{i+1}, \quad 1 \leq i \leq \rho - 1$$

$$\dot{e}_\rho = a(\eta, \xi) + b(\eta, \xi)u + \delta(t, \eta, \xi, u) - r^{(\rho)}(t)$$

Regulation:

$$\dot{\eta} = f_0(\eta, \xi, w)$$

$$\dot{\xi}_i = \xi_{i+1}, \quad 1 \leq i \leq \rho - 1$$

$$\dot{\xi}_\rho = a(\eta, \xi, w) + b(\eta, \xi, w)u$$

$$y = \xi_1$$

- Design partial state feedback control that uses ξ
- Use a high-gain observer

Tracking sliding mode controller:

$$u = -\beta(\xi) \operatorname{sat} \left(\frac{k_1 e_1 + \cdots + k_{\rho-1} e_{\rho-1} + e_{\rho}}{\mu} \right)$$

Regulation sliding mode controller:

$$u = -\beta(\xi) \operatorname{sat} \left(\frac{k_0 e_0 + k_1 e_1 + \cdots + k_{\rho-1} e_{\rho-1} + e_{\rho}}{\mu} \right)$$

$$\dot{e}_0 = e_1 = y - r$$

β is allowed to depend only on ξ rather than the full state vector. On compact sets, the η -dependent part of $\varrho(\eta, \xi)$ can be bounded by a constant

High-gain observer:

$$\dot{\hat{e}}_i = \hat{e}_{i+1} + \frac{\alpha_i}{\varepsilon^i}(y - r - \hat{e}_1), \quad 1 \leq i \leq \rho - 1$$

$$\dot{\hat{e}}_\rho = \frac{\alpha_\rho}{\varepsilon^\rho}(y - r - \hat{e}_1)$$

$$\lambda^\rho + \alpha_1 \lambda^{\rho-1} + \cdots + \alpha_{\rho-1} \lambda + \alpha_\rho \text{ Hurwitz}$$

$$e \rightarrow \hat{e}$$

$$\xi \rightarrow \hat{\xi} = \hat{e} + \mathcal{R}$$

$$\beta(\hat{\xi}) \rightarrow \beta_s(\hat{\xi}) \text{ (saturated)}$$

Tracking:

$$u = -\beta_s(\hat{\xi}) \operatorname{sat} \left(\frac{k_1 \hat{e}_1 + \cdots + k_{\rho-1} \hat{e}_{\rho-1} + \hat{e}_\rho}{\mu} \right)$$

Regulation:

$$u = -\beta_s(\hat{\xi}) \operatorname{sat} \left(\frac{k_0 e_0 + k_1 \hat{e}_1 + \cdots + k_{\rho-1} \hat{e}_{\rho-1} + \hat{e}_\rho}{\mu} \right)$$

We can replace $\hat{e}_1$ by e_1

Special case: When β_s is constant or function of $\hat{e}$ rather than $\hat{\xi}$, we do not need the derivatives of r , as required by Assumption 13.4

The output feedback controllers recover the performance of the partial state feedback controllers for sufficiently small ε . In the regulation case, the regulation error converges to zero

Relative degree one systems: No observer

$$u = -\beta(y) \operatorname{sat} \left(\frac{y - r}{\mu} \right), \quad u = -\beta(y) \operatorname{sat} \left(\frac{k_0 e_0 + y - r}{\mu} \right)$$

Example 13.5 (Revisit Example 13.2 and 13.4)

Use the high-gain observer

$$\dot{\hat{e}}_1 = \hat{e}_2 + \frac{2}{\varepsilon}(e_1 - \hat{e}_1), \quad \dot{\hat{e}}_2 = \frac{1}{\varepsilon^2}(e_1 - \hat{e}_1)$$

to implement the tracking controller

$$u = -(2|e_2| + 3) \operatorname{sat} \left(\frac{e_1 + e_2}{\mu} \right) \quad (\text{Example 13.2})$$

and the regulating controller

$$u = -(2|e_1| + 4|e_2| + 4) \operatorname{sat} \left(\frac{e_0 + 2e_1 + e_2}{\mu} \right) \quad (\text{Example 13.4})$$

Replace e_2 by $\hat{e}_2$ but keep e_1

Saturate $|\hat{e}_2|$ in the β function over a compact set of interest.
There is no need to saturate $\hat{e}_2$ inside the saturation

For Example 13.2,

$$\Omega = \{|e_1| \leq c/\theta\} \times \{|s| \leq c\}, \quad c > 0, \quad 0 < \theta < 1$$

is positively invariant. Take $c = 2$ and $1/\theta = 1.1$

$$\Omega = \{|e_1| \leq 2.2\} \times \{|s| \leq 2\}$$

Over Ω , $|e_2| \leq |e_1| + |s| \leq 4.2$. Saturate $|\hat{e}_2|$ at 4.5

$$u = - \left(2 \times 4.5 \operatorname{sat} \left(\frac{|\hat{e}_2|}{4.5} \right) + 3 \right) \operatorname{sat} \left(\frac{e_1 + \hat{e}_2}{\mu} \right)$$

For Example 13.4,

$$\dot{\zeta} = A\zeta + Bs, \quad \zeta = \begin{bmatrix} e_0 \\ e_1 \end{bmatrix}, \quad A = \begin{bmatrix} 0 & 1 \\ -1 & -2 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$PA + A^T P = -I, 0 < \theta < 1, \rho_1 = \lambda_{\max}(P)(2\|PB\|/\theta)^2, c > 0$$

$$\Omega = \{\zeta^T P \zeta \leq \rho_1 c^2\} \times \{|s| \leq c\}$$

is positively invariant. Take $c = 4$ and $1/\theta = 1.003$

$$\Omega = \{\zeta^T P \zeta \leq 55\} \times \{|s| \leq 4\}$$

Over Ω ,

$$|e_0 + 2e_1| \leq 22.25 \Rightarrow |e_2| \leq |e_0 + 2e_1| + |s| \leq 26.25$$

Saturate $|\hat{e}_2|$ at 27

$$u = - \left(2|e_1| + 4 \times 27 \operatorname{sat} \left(\frac{|\hat{e}_2|}{27} \right) + 4 \right) \operatorname{sat} \left(\frac{e_0 + 2e_1 + \hat{e}_2}{\mu} \right)$$

Simulation; (a) Tracking, (b) regulation

$$\varepsilon = \begin{cases} 0.05 & \text{(dashed)} \\ 0.01 & \text{(dash-dot)} \end{cases}$$

State feedback (solid)

